

# Lesson 11: Separately Excited Motor Examples

ET 332a

Dc Motors, Generators and Energy Conversion Devices

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## Learning Objectives

After this presentation you will be able to:

- Write a power balance for a separately excited motor and compute its efficiency
- Explain how changing motor load affects efficiency
- Interpret motor nameplate data

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## Power Relationships for Dc Motors

The electromechanical power output from the armature is equal to the total electrical power input to the armature

KVL in armature circuit gives  $V_T = I_a \cdot R_{acir} + E_a$

Multiply by  $I_a$   $V_T \cdot I_a = I_a^2 \cdot R_{acir} + E_a I_a$

From generator power balance  $P_{em} = E_a \cdot I_a$

$$P_e = E_a \cdot I_a$$

Where:  $P_{em}$  = the mechanical power developed in the armature and  
 $P_e$  is the electrical power input to the motor

Combining above equations gives  $P_{em} = V_T \cdot I_a - I_a^2 \cdot R_{acir}$

Where:  $R_{acir} = R_a + R_{IP} + R_{CW}$

$R_a$  = armature resistance  $R_{CW}$  = compensating winding resistance  
 $R_{IP}$  = interpole resistance

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## Motor Nameplate Ratings

Motor nameplate data is given in horsepower (hp) and revolutions per minute (RPM).

All motor characteristics are standardized by National Electrical Manufacturers Association (NEMA)

**Physical characteristics** - size, dimensions shaft placement, etc.

**Electrical characteristics** - voltage rating torque/speed characteristics.

HP ratings

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## Motor Nameplate Ratings

At rated voltage and current, motor delivers rated HP at rated speed.

Relationship between torque and mechanical power at shaft in terms of mechanical units.

$$P_{\text{shaft}} = \frac{T_{\text{shaft}} \cdot n}{5252} \text{ Hp}$$

Where:  $T_{\text{shaft}}$  = developed torque at motor shaft (lb-ft)

$n$  = shaft speed (rpm)

$P_{\text{shaft}}$  = shaft power output (hp)

Armature torque and power must be larger to overcome mechanical losses

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## Example 11-1 Shaft Power Calculations

A 15 Hp separately excited motor is operating at its rated speed of 1200 rpm. Determine the rated torque of the motor in ft-lbs.

**Solution** Rated mechanical power output  $P_{\text{shaft}} = 15 \text{ hp}$

$n = 1200 \text{ rpm}$  Rated speed

$$P_{\text{shaft}} = \frac{T_{\text{rated}} n}{5252} \Rightarrow \frac{P_{\text{shaft}} 5252}{n} = T_{\text{rated}}$$

$$\frac{(15 \text{ hp})(5252)}{1200 \text{ rpm}} = T_{\text{shaft}}$$

$$65.65 \text{ lb-ft} = T_{\text{shaft}}$$

This is smaller than the actual torque developed at the armature

$$T_w = E_a I_a$$

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## Example 11-2 Torque Constant

A 25 Hp separately excited motor is operating at a speed of 250 rpm. It is supplied from a 120V supply and draws 5.6 A. The total armature circuit resistance is .473 ohms. Find the torque constant for the machine

$$E_a = V_t - I_a R_{a+c} \quad E_a = 120V - (5.6A)(0.473\Omega) = 117.35V$$

$$P_e = E_a I_a = (117.35V)(5.6A) = 657.17W$$

$$P_{em} = P_e \quad P_{em} = T \omega$$

Convert rpm to rad/sec  $\omega = \frac{2\pi}{60} (250 \text{ rpm}) = 26.167 \text{ rad/s}$

Find the torque

$$\frac{P_{em}}{\omega} = T \quad \frac{657.17W}{26.167 \text{ rad/sec}} = \boxed{25.1 \text{ N}\cdot\text{m}}$$

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## Example 11-2 Torque Constant (2)

Remember

$$T = B_p I_a K_G \Rightarrow \frac{T}{I_a} = B_p K_G$$

$B_p$  is constant for constant field current. So .....

$$B_p K_G = K_T$$

$K_T$  is the motor torque constant

$$\frac{25.11 \text{ N}\cdot\text{m}}{5.6 \text{ A}} = B_p K_G = 4.485 \frac{\text{N}\cdot\text{m}}{\text{A}}$$

**Note:**  $K_T$  is numerically equal to  $K_e$  when using SI units.  
In this case  $K_e = 4.485 \text{ V}\cdot\text{sec/rad}$

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## General Speed Equations for Dc Motors

Remember  $E_a = V_T - I_a \cdot R_{acir}$        $n = \frac{E_a}{\Phi_p \cdot K_G}$

Combine the two above to get speed equation

$$n = \frac{V_T - I_a \cdot R_{acir}}{\Phi_p \cdot K_G}$$

Where:  $R_{acir}$  = armature circuit resistance

$I_a$  = armature current

$K_G$  = machine constant

$n$  = speed (rpm)

$\Phi_p$  = field flux

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## General Speed Equations for Dc Motors

Speed inversely proportional to the field flux. Decreasing the field flux increases speed **providing sufficient torque is developed to produce necessary acceleration.**

Remember  $T_D = k_T \cdot I_f \cdot I_a$

$$n = \frac{V_T - I_a \cdot R_{acir}}{\Phi_p \cdot K_G}$$

Decreasing  $I_f$  reduces field flux but also reduces developed torque

Controlled by  $I_f$

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## Motor Speed and Terminal Voltage

Motor speed is directly proportional to the terminal voltage. Increasing  $V_T$  increases  $n$ , Decreasing  $V_T$  decreases  $n$

**Example 11-3:** A 50 HP, 240 Vdc separately excited motor is operating at 1000 rpm. The motor draws 7800 watts from dc supply. The total armature resistance is 0.221  $\Omega$ . Find:

- The emf constant,  $K_e$  of the motor
- The motor speed if the terminal voltage is reduced by 20% and the power drawn remains the same.

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## Example 11-3 Solution (1)

**Part a.)**

$$n = \frac{V_T - I_a R_{acir}}{\Phi_p K_e} \quad \text{Remember } \Phi_p K_e = K_e$$

$K_e = \text{emf constant}$

$$n = 1000 \text{ rpm} \quad V_T = 240 \text{ V} \quad R_{acir} = 0.221 \Omega$$

$$\text{Find } I_a \quad P_e = V_T I_a \quad \text{electrical input power}$$

$$\frac{P_e}{V_T} = I_a \Rightarrow \frac{7800 \text{ W}}{240 \text{ V}} = I_a \quad n = \frac{V_T - I_a R_{acir}}{K_e} \quad K_e = \frac{240 \text{ V} - (32.5 \text{ A})(0.221 \Omega)}{1000 \text{ rpm}}$$

$$32.5 \text{ A} = I_a \quad K_e = \frac{V_T - I_a R_{acir}}{n} \quad \boxed{K_e = 0.2328 \text{ V/rpm}}$$

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## Example 11-3 Solution (2)

**Part b.**  $K_e$  remains the same, no change in the field current

$$V_{T2} = V_T - V_T \left( \frac{200\%}{1000\%} \right) \quad V_{T2} = 240 - 240(0.20) = 192V$$

$P_e$  Remains constant  $\frac{P_{in}}{V_{T2}} = I_{a2} \frac{7800W}{192V} = 40.625A$

$$n_2 = \frac{V_{T2} - I_{a2} R_{acir}}{K_e} = \frac{192V - (40.625A)(0.221A)}{0.2328 \text{ V/rpm}}$$

$$n_2 = 786.2 \text{ rpm}$$

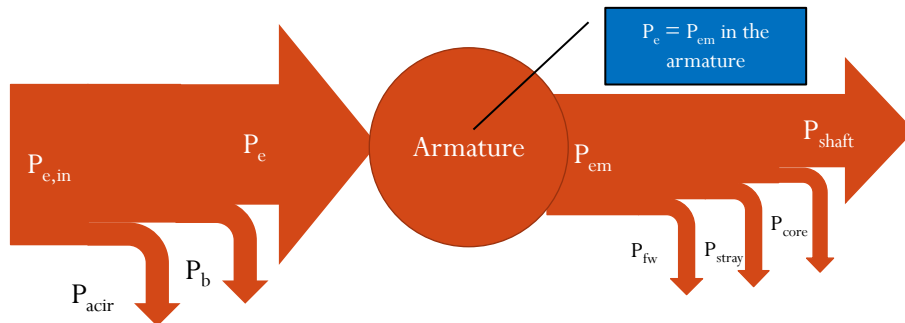
Calculate % speed change

$$\frac{1000 - 786.2}{1000} \times 100\% = 21.3\%$$

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## Power Balance In Dc Motors



- $P_{e,in}$  = electric power in at terminals (W)
- $P_{acir}$  = armature circuit losses  $I_a^2(R_{acir})$  (W)
- $P_b$  = losses due to brush drop  $V_b(I_a)$  (W)
- $P_e$  = electric power delivered to armature ( $E_a$ )- $I_a$  circuit (W)
- $P_{em}$  = Electromechanical power developed in armature ( $T_d$ )- $\omega$  (W)

- $P_{fw}$  = friction and windage losses (W) (from test)
- $P_{stray}$  = stray load losses (W) (from test)
- $P_{core}$  = core losses (W) (from test)
- $P_{shaft}$  = total mechanical power develop at the shaft (Rated hp)

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$P_{fw} + P_{stray} + P_{core}$  are called rotational losses

## Motor Efficiency

Remember from generators

$$\eta = \left[ \frac{P_{\text{out}}}{P_{\text{in}}} \right] \cdot 100\%$$

Just like generators, efficiency varies with motor  $P_{\text{shaft}}$ . Nameplate efficiency occurs at rated output.

For motors:  
 $P_{\text{out}} = P_{\text{shaft}}$  mechanical power developed at the shaft  
 $P_{\text{in}} = P_{\text{e,in}}$  the electrical power supplied to the terminals  
 $\eta$  = percent efficiency

In terms of losses  $P_{\text{losses}} = P_{\text{acir}} + P_{\text{b}} + P_{\text{fw}} + P_{\text{core}} + P_{\text{stray}}$

Where  $P_{\text{acir}}$  = armature circuit losses  
 $P_{\text{b}}$  = brush losses  
 $P_{\text{fw}}$  = friction and windage losses  
 $P_{\text{core}}$  = core losses  
 $P_{\text{stray}}$  = stray losses

$$\eta = \left[ \frac{P_{\text{out}}}{P_{\text{out}} + P_{\text{losses}}} \right] \cdot 100\%$$

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## Example 11-4 Motor Solutions Using Efficiency

A separately excited dc motor is rated at 100 HP, 600 V at 1200 rpm. The total armature resistance is 0.24 ohms. When the motor is delivering 75 HP at 1200 rpm its efficiency is 88%. At the 75 HP output find:

- the motor armature current
- counter emf ( $E_a$ )
- torque at the shaft
- an estimate of the mechanical losses

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## Example 11-4 Solution (1)

a.) Find the armature current. Use efficiency to relate  $P_{\text{shaft}}$  to  $P_{e,\text{in}}$

$$P_{\text{out}} = 75 \text{ hp} \left[ \frac{746 \text{ W}}{1 \text{ hp}} \right] = 55,950 \text{ W}$$

$$\eta = \left[ \frac{P_{\text{out}}}{P_{e,\text{in}}} \right] 100\% \quad \eta = 88\%$$

$$P_{e,\text{in}} = \frac{P_{\text{out}}}{\eta/100} = \frac{55,950 \text{ W}}{88/100}$$

$$P_{e,\text{in}} = 63,580 \text{ W}$$

$$V_T = 600 \text{ V}$$

$$I_a = \frac{P_{e,\text{in}}}{V_T} = \frac{63,580 \text{ W}}{600 \text{ V}}$$

$$I_a = 106 \text{ A}$$

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## Example 11-4 Solution (2)

b.) Find  $E_a$ . Use the current from part a to find the emf

$$V_T = E_a + I_a R_{a,c,r} \Rightarrow V_T - I_a R_{a,c,r} = E_a$$

$$E_a = 600 \text{ V} - (0.21 \Omega)(106 \text{ A}) = 579.6 \text{ V}$$

c.) Find shaft torque (N-m). Use rated Hp and speed

$$P_{\text{out}} = P_{\text{shaft}} = 55,950 \text{ W} \quad \text{Part a}$$

Convert speed to rad/sec

$$1200 \text{ rpm} \left[ \frac{2\pi}{60} \right] = 125.7 \text{ rad/s}$$

$$T_{\text{shaft}} = \frac{P_{\text{shaft}}}{\omega} = \frac{55,950 \text{ W}}{125.7 \text{ rad/s}} = 445.2 \text{ N-m}$$

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## Example 11-4 Solution (3)

d.) Estimate the rotational losses (mechanical losses)

MECHANICAL LOSSES

$$P_{fw} + P_{core} + P_{stray}$$

$$P_{fw} + P_{core} + P_{stray} = P_{em} - P_{shaft}$$

$$P_{em} = P_e = E_a I_a \quad E_a = 579.6 \text{ V}$$

$$I_a = 106 \text{ A}$$

$$P_{em} = (579.6 \text{ V})(106 \text{ A}) = 60,907.6 \text{ W}$$

$$60,907.6 \text{ W} - 55,950 \text{ W} = 4957.6 \text{ W}$$

About 6.6 hp

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## End Lesson 11

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