

Lesson 22_et332b.pptx

LESSON 22: ACTIVE POWER DIVISION BETWEEN ALTERNATORS

ET 332b
Ac Motors, Generators and Power Systems

LEARNING OBJECTIVES

After this presentation you will be able to:

- Explain how active power load divides between parallel alternators with equal governor droop
- Explain how active power load divides between parallel alternators with unequal governor droop
- Define isochronous governor operation
- Compute the load division and system frequency of a load increase on parallel generators.

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2

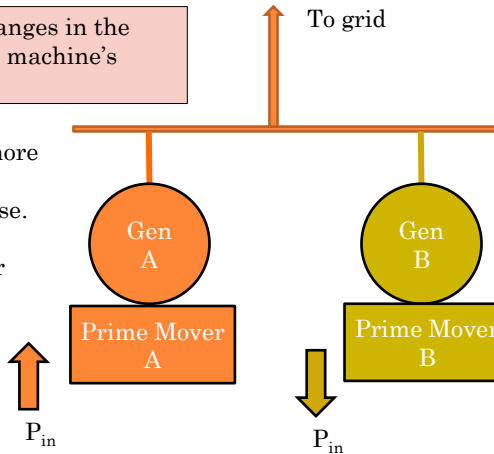
ACTIVE POWER DIVISION BETWEEN ALTERNATORS

Governor droop determines the active power division between parallel alternators

Load shifting requires changes in the mechanical power of each machine's prime-mover

If Gen A wishes to take more active power load, prime-mover power must increase.

Gen B prime-mover power must decrease or system frequency will increase.



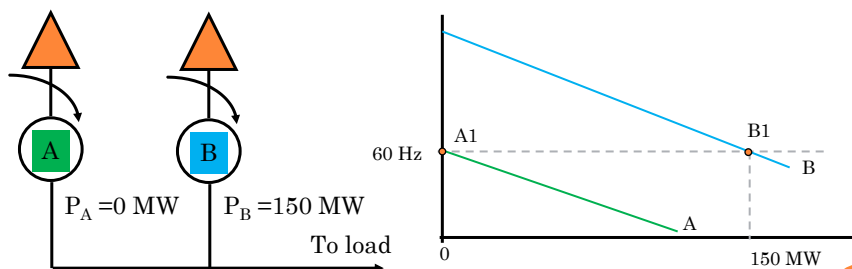
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3

ACTIVE POWER DIVISION BETWEEN ALTERNATORS

Power transfer between alternators accomplished by adjusting their governor's no-load speed settings

Example 22-1: Two alternators serve a 150 MW load in an isolated power system and have identical governor characteristics



Initial conditions:

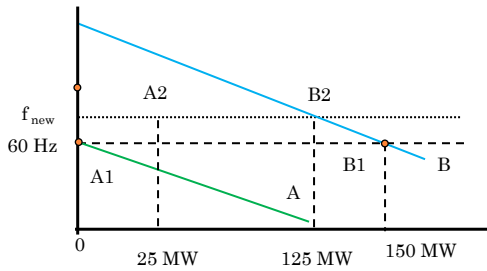
Frequency is constant in power system. Change load by shifting governor characteristics.

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4

ACTIVE POWER DIVISION BETWEEN ALTERNATORS

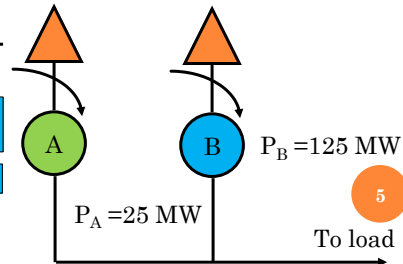
To shift load: raise the no-load speed of Gen A raising the whole characteristic.



If 50 MW change required, pick up 25 MW on Gen A

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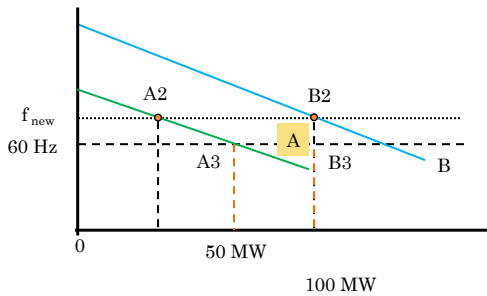
- Speed increases on A because more mechanical power is applied to the prime-mover
- Speed increases on B because load transfers to A from B



5

ACTIVE POWER DIVISION BETWEEN ALTERNATORS

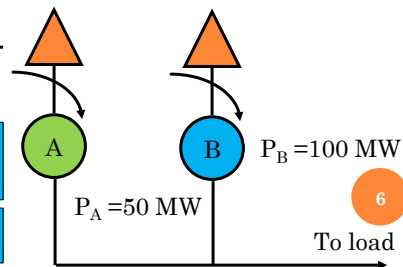
System frequency must remain at 60 Hz so Gen B must lower its characteristic



Gen B lowers characteristic to reduce load by 25 MW

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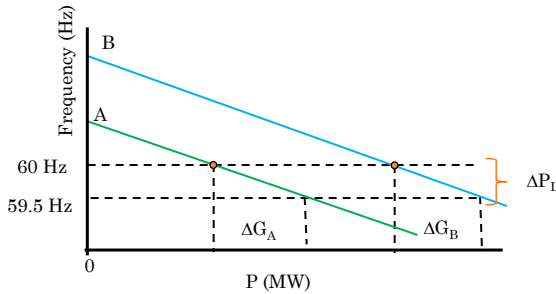
- Machines with identical governor droops divide load increases equally between themselves regardless of machine rating
- With dissimilar governor droops machine with least droop assumes most of any load change



6

LOAD INCREASE AND SYSTEM FREQUENCY

If electrical load on system increases and there is no governor control the system frequency falls



Adding load to a system with similar governor droops

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Automatic control of governor no-load speed corrects for change in load by raising or lowering the characteristics of the machines. This causes the development of more or less mechanical power.
 Steam Turbines – open turbine control valve more
 Diesel Engine – open throttle more
 Hydropower – open water control valves

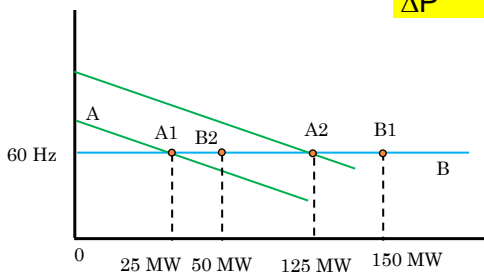
7

ISOCHRONOUS GOVERNORS AND FREQUENCY CONTROL

Isochronous governors - This type of governor can maintain constant speed for any level of output power.

For isochronous governors

$$\frac{\Delta f}{\Delta P} = 0$$



Gen B is isochronous

Can only change loading by changing A's characteristic. Changing B changes system frequency. Isochronous machine takes load changes.

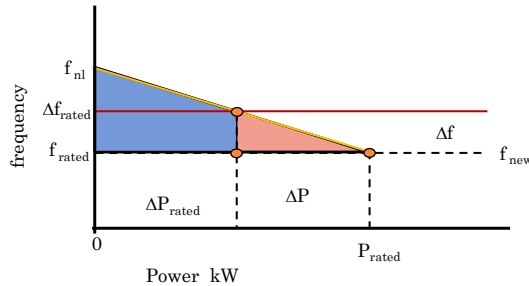
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- 1.) $P_A = 25 \text{ MW}$, $P_B = 150 \text{ MW}$ $P_T = P_A + P_B = 25 + 150 = 175 \text{ MW}$
- 2.) $P_A = 125 \text{ MW}$, $P_B = 50 \text{ MW}$ $P_T = P_A + P_B = 125 + 50 = 175 \text{ MW}$

8

POWER DIVISION IN PARALLEL ALTERNATORS

Use similar triangle solution to find active power distribution in parallel alternators



From Similar Triangles

$$GD = \frac{f_{nl} - f_{rated}}{P_{rated}}$$

So

$$\frac{f_{nl} - f_{rated}}{P_{rated}} = \frac{\Delta f}{\Delta P}$$

Rearranging the speed regulation equation gives:

$$GD = \frac{GSR \cdot f_{rated}}{P_{rated}} = \frac{\Delta f}{\Delta P}$$

Where: GD = governor droop
 GSR = governor speed regulation
 Δf = change in f due to change in load
 ΔP = change in load

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9

Example 22-1: Parallel generators A and B share a total load of 300 kW at 60 Hz.

Machine	Voltage	Power	GSR	Freq	Load
A	460 V	500 kW	2.0%	60 Hz	100 kW
B	460 V	500 kW	2.0%	60 Hz	200 kW

If generator A trips off line determine a.) frequency of generator A b.) frequency of generator B c.) frequency of the system

Qualitative analysis: Machine A loses load and should have speed increase. Machine B must take up load lost by A and should decrease speed.

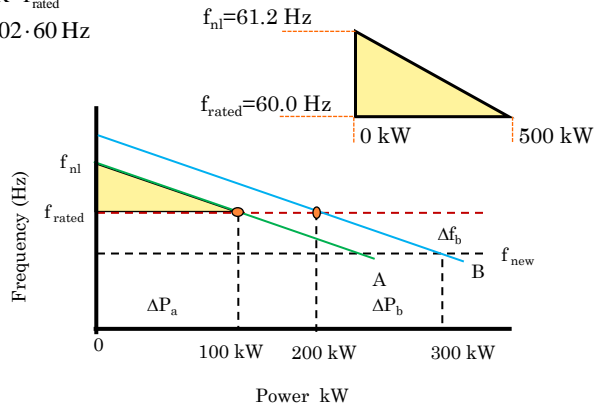
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10

EXAMPLE 22-1 SOLUTION (1)

Show system operation using power/frequency plots

$$\begin{aligned} f_{nl} &= f_{\text{rated}} + \text{GSR} \cdot f_{\text{rated}} \\ f_{nl} &= 60 \text{ Hz} + 0.02 \cdot 60 \text{ Hz} \\ f_{nl} &= 61.2 \text{ Hz} \end{aligned}$$



After A trips off-line $P_A=0$ and $P_B=300 \text{ kW}$
 $\Delta P_A=\Delta P_B=100 \text{ kW}$

11

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EXAMPLE 22-1 SOLUTION (2)

a.) For machine A

$$\frac{\text{GSR} \cdot f_{\text{rated}}}{P_{\text{rated}}} = \frac{\Delta f_a}{\Delta P_a}$$

$\Delta P_a = 100 \text{ kW}$ A tripped off. Now delivers 0 kW

$$\frac{0.02 \cdot 60 \text{ Hz}}{500 \text{ kW}} = \frac{\Delta f_a}{100}$$

$$\Delta f_a = 0.24 \text{ Hz}$$

$$f_a = 60 + 0.24 = 60.24 \text{ Hz}$$



Loss of electrical load causes speed to increase if mechanical power input is not decreased.

12

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EXAMPLE 22-1 SOLUTION (3)

b.) Since Gen A and B are identical, increasing electrical load causes frequency to drop if mechanical power input is not increased

$$f_b = 60 - 0.24 = 59.76 \text{ Hz} \quad \leftarrow \text{Answer}$$

c.) Only Gen B is on-line, so its frequency is the system frequency

$$f_s = 59.76 \text{ Hz} \quad \leftarrow \text{Answer}$$

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13

Example 22-2: 500 kW 60 Hz 2300 V alternator is paralleled with a 60 Hz 300 kW machine. Both have governor speed regulation values of 2.43%. Each machine carries 200 kW at a frequency of 60.5 Hz. If total load increases to 500 kW determine:

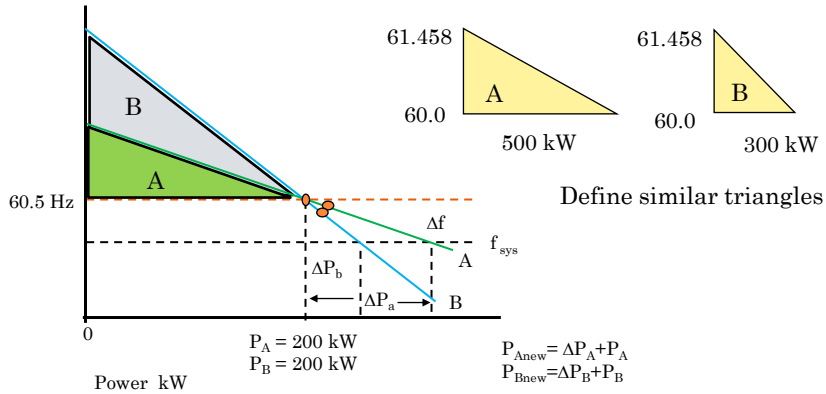
- a.) system frequency
- b.) load carries by each machine

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14

EXAMPLE 22-2 SOLUTION (1)

Machines have unequal governor droops.



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Increasing load causes machines to follow governor curves

15

EXAMPLE 22-2 SOLUTION (2)

FOR EACH MACHINE:

$$\frac{GSR \times f_{rated}}{P_{rated}} = \frac{\Delta f}{\Delta P}$$

In this case ΔP & Δf are unknown

$$P_{ratedA} = 500 \text{ kW} \quad f_{ratedA} = f_{ratedB} = 60 \text{ Hz}$$

$$P_{ratedB} = 300 \text{ kW} \quad GSR_A = GSR_B = 0.0243$$

So for MACHINE A

$$\frac{0.0243(60 \text{ Hz})}{500 \text{ kW}} = \frac{\Delta f_s}{\Delta P_A}$$

$$\Delta P_A = 342.936 \Delta f_s$$

MACHINE B

$$\frac{0.0243(60 \text{ Hz})}{300 \text{ kW}} = \frac{\Delta f_s}{\Delta P_B}$$

$$\Delta P_B + 205.761 \Delta f_s$$

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16

EXAMPLE 22-2 SOLUTION (3)

$$\Delta P_A + \Delta P_B = \Delta P_L$$

$\Delta P_L =$ change in system load

$$(500 \text{ kW} - 400 \text{ kW}) = \Delta P_L$$

$$\Delta P_A + \Delta P_B = 342.936 \Delta f_s + 205.761 \Delta f_s = 500 - 400 \text{ kW}$$

$$548.697 \text{ Hz/kW} \Delta f_s = 100 \text{ kW}$$

$$\Delta f_s = 0.182 \text{ Hz}$$

Increase in load
causes f decrease

$$f_s = f_{\text{init}} - \Delta f_s \quad f_{\text{init}} = 60.5 \text{ Hz}$$

$$f_s = 60.5 \text{ Hz} - 0.182 \text{ Hz} = \boxed{60.318 \text{ Hz}}$$

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17

EXAMPLE 22-2 SOLUTION (4)

ΔP_A and ΔP_B found from original relationships

$$\Delta P_A = 342.936 \Delta f = 342.936 (0.182) = 62.414 \text{ kW}$$

$$\Delta P_B = (205.761 \text{ Hz/kW})(0.182 \text{ Hz}) = 37.586 \text{ kW}$$

OR

$$\Delta P_L = 100 \text{ kW} \quad \Delta P_L = \Delta P_A + \Delta P_B$$

$$\text{SO } \Delta P_B = \Delta P_L - \Delta P_A$$

$$\Delta P_B = 100 \text{ kW} - 62.414 \text{ kW}$$

$$\Delta P_B = 37.586 \text{ kW}$$

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18

EXAMPLE 22-2 SOLUTION (5)

$$P_{A\text{new}} = P_A + \Delta P_A = 200 \text{ kW} + 62.414 \text{ kW}$$

$$P_{A\text{new}} = 262.414 \text{ kW}$$

$$P_{B\text{new}} = P_B + \Delta P_B = 200 \text{ kW} + 37.59 \text{ kW}$$

$$P_{B\text{new}} = 237.59 \text{ kW}$$

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19

END LESSON 22: ACTIVE POWER DIVISION BETWEEN ALTERNATORS

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20

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