

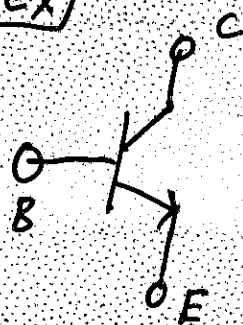
Methods of Analysis

Current Sources

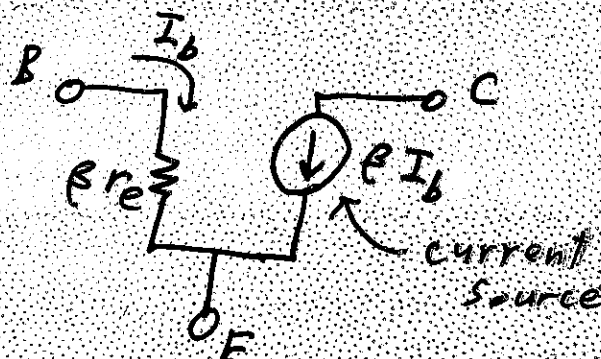
A current source determines the current in the branch in which it is located.

The magnitude and polarity of the voltage across a current source are a function of the network to which it is applied.

ex/

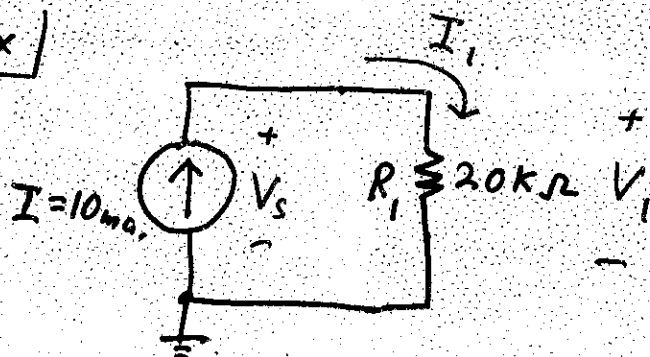


Transistor



Transistor's equivalent circuit

ex/

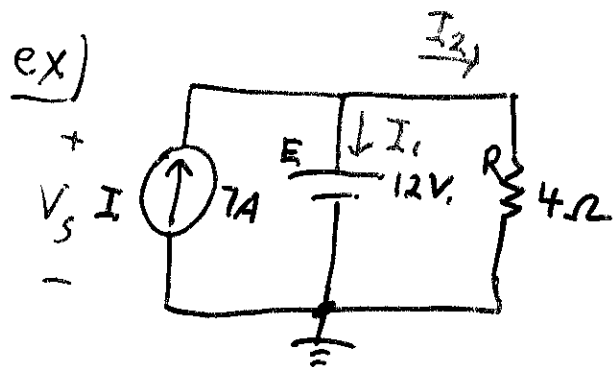


Find V_s and I_1 .

$$I_1 = I = 10 \text{ mA}$$

$$V_s = V_1 = I_1 R_1 = (10 \text{ mA})(20 \text{ k}\Omega) = 200 \text{ V}$$

ex)



Find V_s , I , and I_2

$$V_s = E = 12V$$

By Ohm's Law:

$$I_2 = \frac{V_R}{R} = \frac{E}{R} = \frac{12V}{4\Omega} = 3A$$

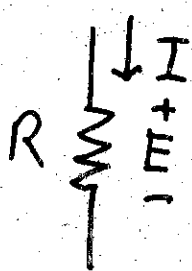
By Kirchhoff's Current Law (KCL):

$$I = I_1 + I_2$$

so $I_1 = I - I_2 = 7A - 3A = 4A$

Ohm's Law:

Given the voltage polarity and current direction shown in the diagram:

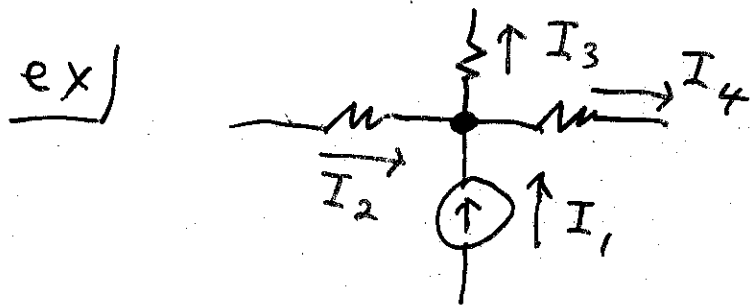


$$I = \frac{E}{R}, \quad E = IR$$

Note: The current is entering the positively labelled voltage terminal.

Kirchhoff's Current Law (KCL):

The sum of the currents leaving a circuit node is equal to the sum of the currents entering the circuit node.

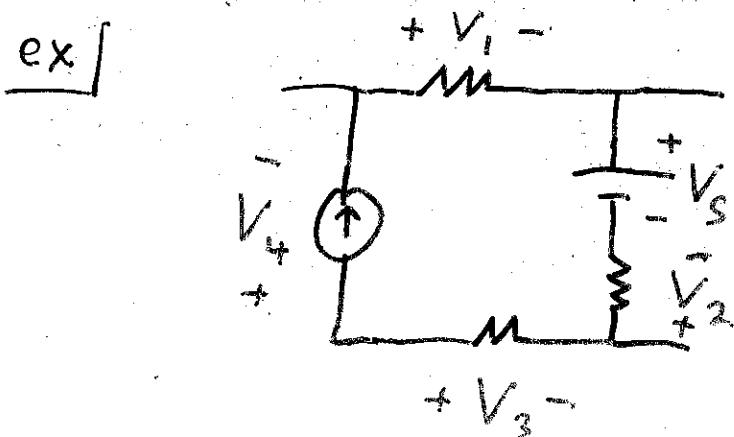


By KCL:

$$I_3 + I_4 = I_1 + I_2$$

Kirchhoff's Voltage Law (KVL):

The algebraic sum of the voltages around a completed circuit path must equal zero.

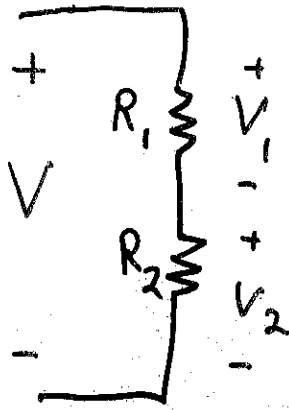


By KVL:

$$V_1 + V_5 - V_2 - V_3 + V_4 = 0$$

Voltage Divider Rule :

Given resistors in series (same current through them) the voltage will divide as follows:

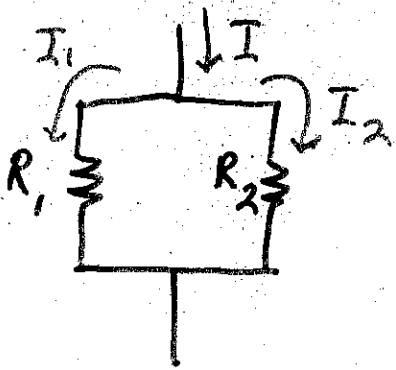


$$V_1 = V \frac{R_1}{R_1 + R_2}$$

$$V_2 = V \frac{R_2}{R_1 + R_2}$$

Current Divider Rule :

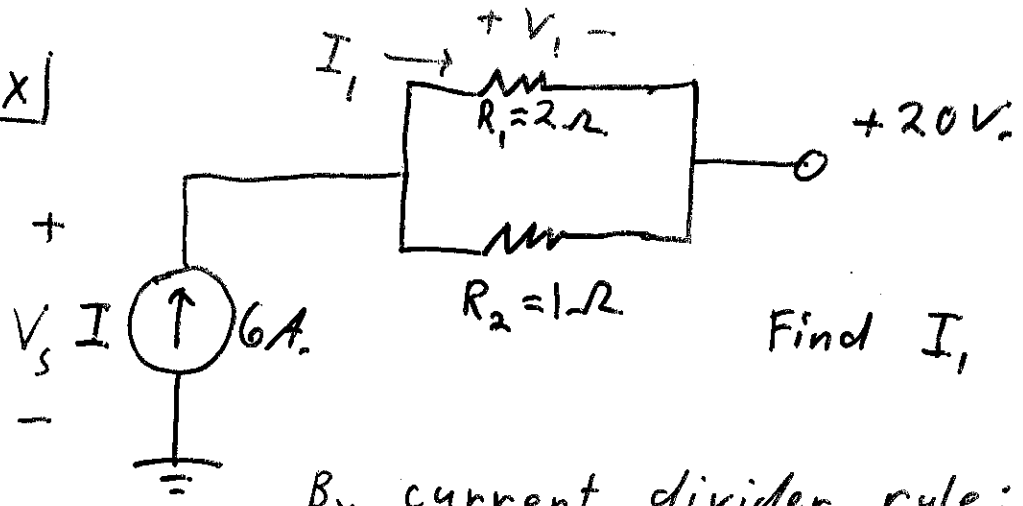
Given resistors in parallel (same voltage across them) the current will divide as follows:



$$I_1 = I \frac{R_2}{R_1 + R_2}$$

$$I_2 = I \frac{R_1}{R_1 + R_2}$$

ex]



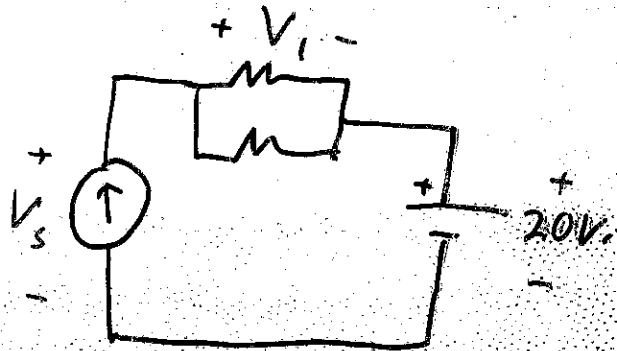
By current divider rule:

$$I_1 = I \frac{R_2}{R_1 + R_2} = \frac{(1\Omega)(6A)}{1\Omega + 2\Omega} = \boxed{2A}$$

By Ohm's Law: $V_1 = I_1 R_1 = (2A)(2\Omega) = 4V$

By KVL:

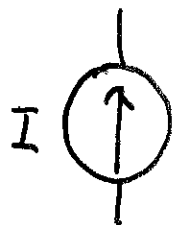
equiv.
ckt. $\Rightarrow$



$$V_1 + 20 - V_s = 0$$

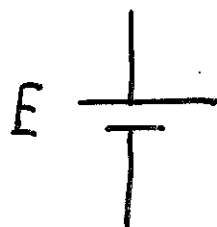
$$V_s = V_1 + 20 = 4 + 20 = \boxed{24V}$$

Source Conversions



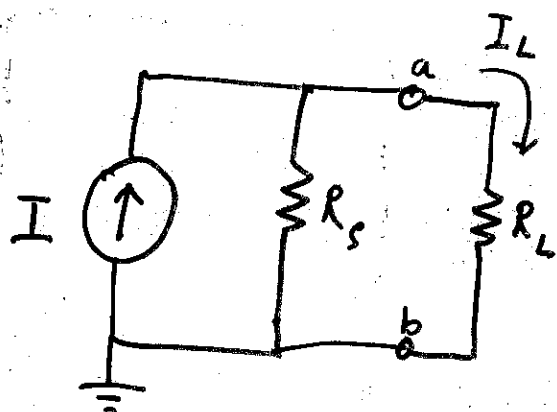
Ideal Current Source

$$R_s = \infty$$



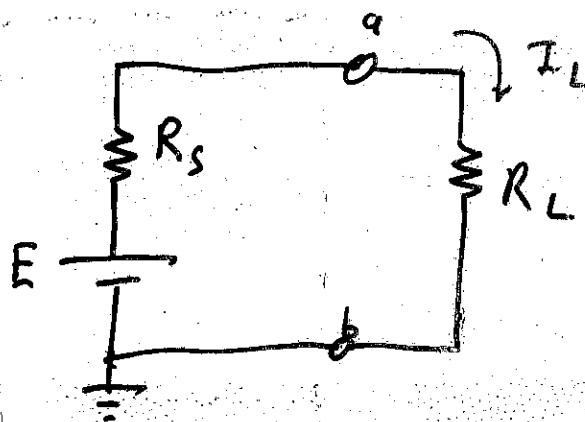
Ideal Voltage Source

$$R_s = 0$$



Practical Current Source

$$I_L = \frac{I R_s}{R_s + R_L}$$



Practical Voltage Source

$$I_L = \frac{E}{R_s + R_L}$$

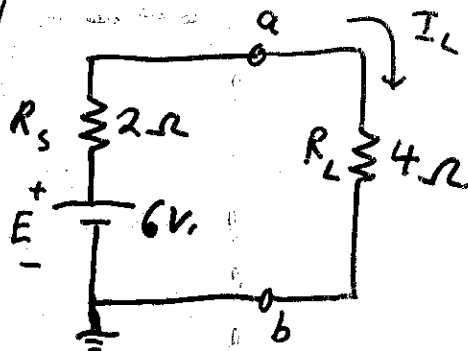
The practical current and voltage sources are equivalent if

$$E = I R_s \quad \text{and} \quad I = \frac{E}{R_s}$$

and measurements taken at terminals a and b can not tell them apart.

Equivalent circuits may be substituted for one another to simplify the circuit analysis.

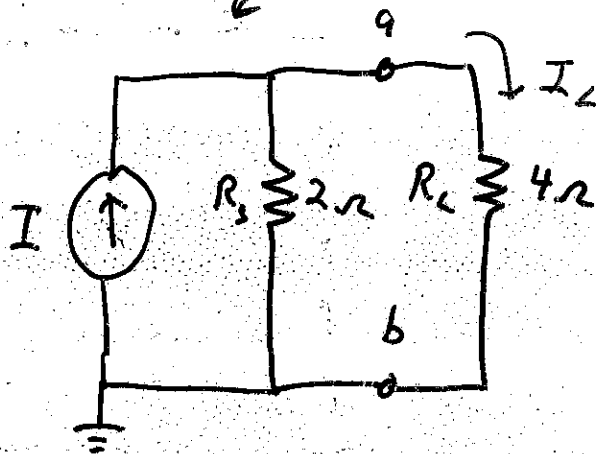
ex/



Find I_L

$$I_L = \frac{E}{R_s + R_L} = \frac{6}{2 + 4} = \boxed{1A}$$

The voltage source could be replaced by an equivalent current source to solve the problem.



$$I = \frac{E}{R_s} = \frac{6}{2} = 3A$$

Then by CDR:

$$I_L = I \frac{R_s}{R_s + R_L} = \frac{3(2)}{2 + 4} = \boxed{1A}$$

If $R_L \gg R_s$, then the practical voltage source model will act like an ideal voltage source ($R_s = 0$).

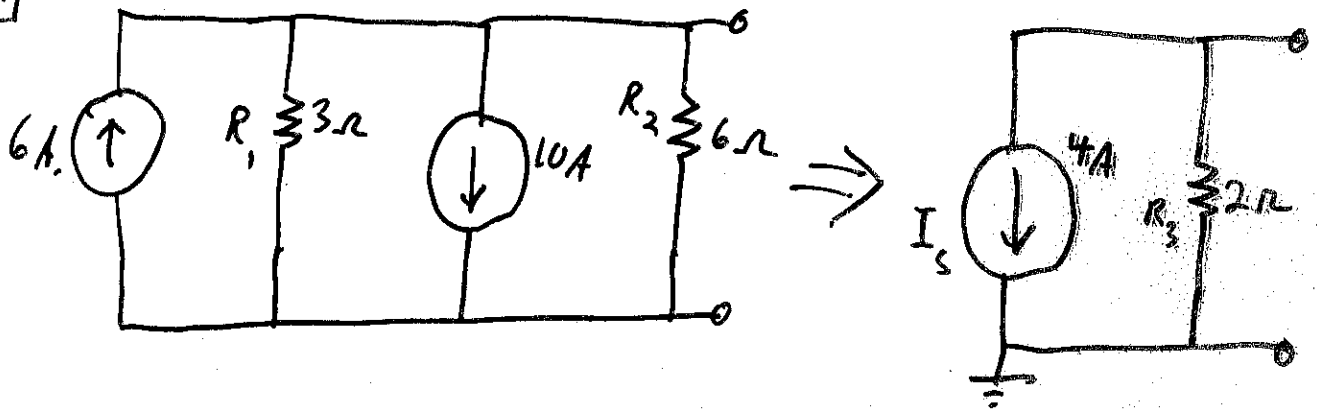
ex/ Given $R_s = 2\Omega$ and $R_L = 1k\Omega$

$$I_L = \frac{E}{R_s + R_L} = \frac{6}{2 + 1k} = 5.99 \mu A$$

Assuming $R_s = 0$ gives: $I_L = \frac{E}{R_L} = \frac{6}{1k} = 6 \mu A \approx 5.99 \mu A$

Two current sources connected in parallel may be replaced by a single current source whose value is their algebraic sum.

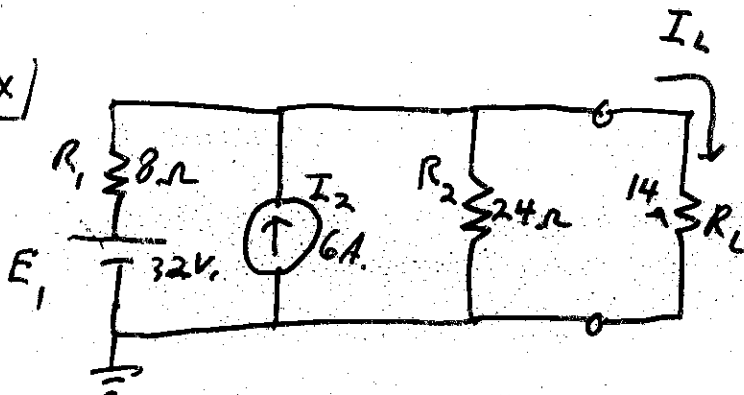
ex/



$$I_s = 10A - 6A = 4A$$

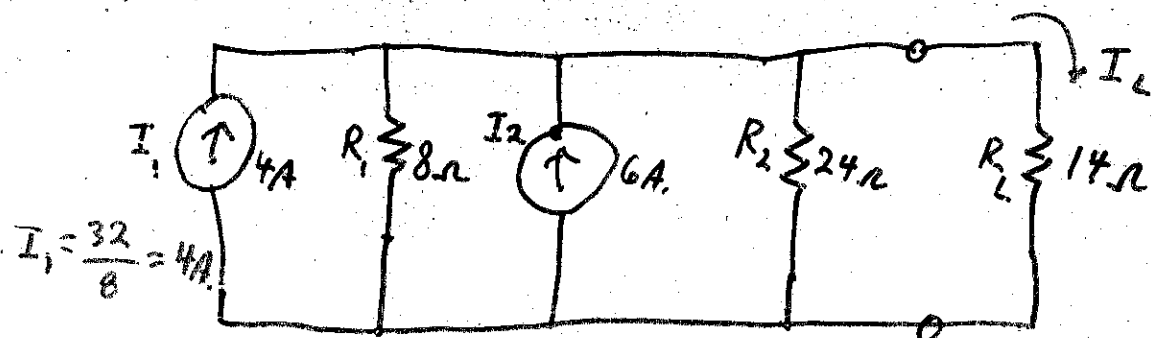
$$R_s = 3\Omega \parallel 6\Omega = 2\Omega$$

ex/

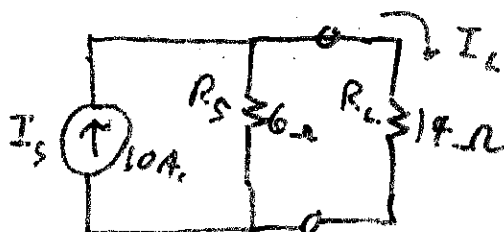


Reduce ckt. to a single current source and find I_L

First convert the voltage source to a current source



Then combine current sources.



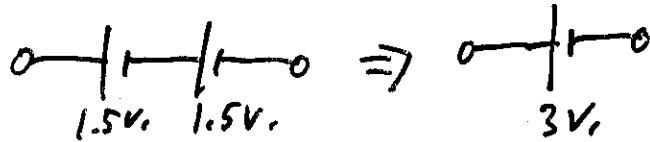
$$I_s = 6 + 4 = 10A, \quad R_s = 8 \parallel 24 = 6\Omega$$

By CDR:

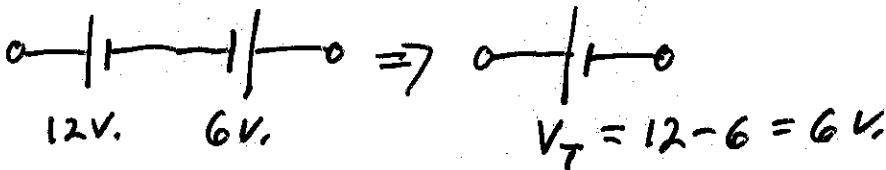
$$I_L = \frac{10(6)}{6+14} = \boxed{3A}$$

Two voltage sources connected in series may be replaced by a single voltage source whose value is their algebraic sum.

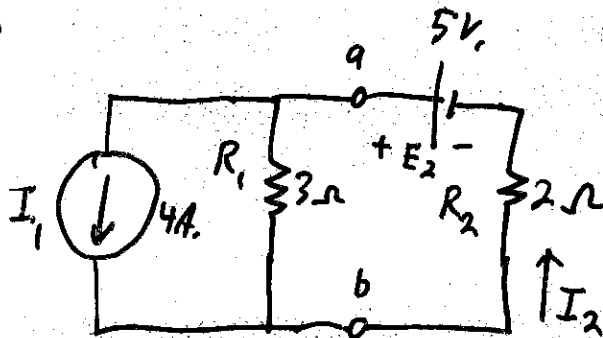
ex/



ex/

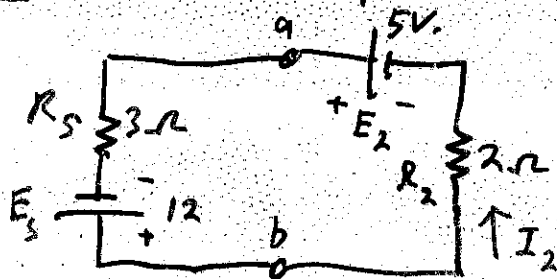


ex/



Find I_2

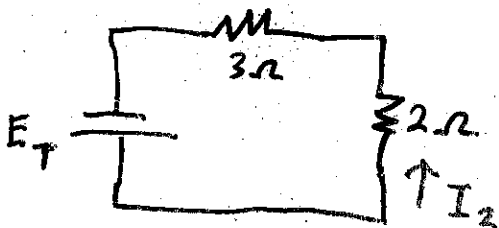
Sol: Convert I_1 into a voltage source



$$E_3 = I_1 R_1 = (4)(3) = 12V$$

$$R_3 = R_1 = 3\Omega$$

Combine voltage sources:



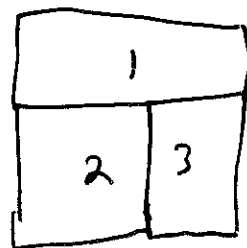
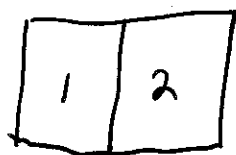
$$E_T = 12 + 5 = 17V$$

$$I_2 = \frac{17}{3 + 2} = \boxed{3.4A}$$

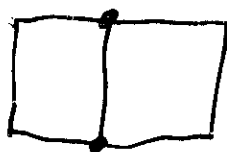
Branch-Current Analysis

1. Assign a current of arbitrary direction to each branch of the network.
2. Label the voltage polarities across each resistor such that the positive side is where the assigned current enters.
3. Apply KVL around each closed circuit path. (loop)
4. Apply KCL at the minimum number of nodes that will include all the branch currents of the network. ($\# \text{KCLs} = \# \text{nodes} - 1$)
5. Solve the resulting simultaneous equations for the assumed branch currents.

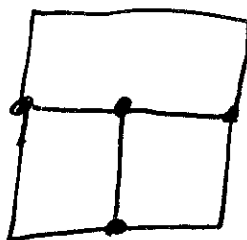
ex/ closed loops;



ex/ required node eqns.

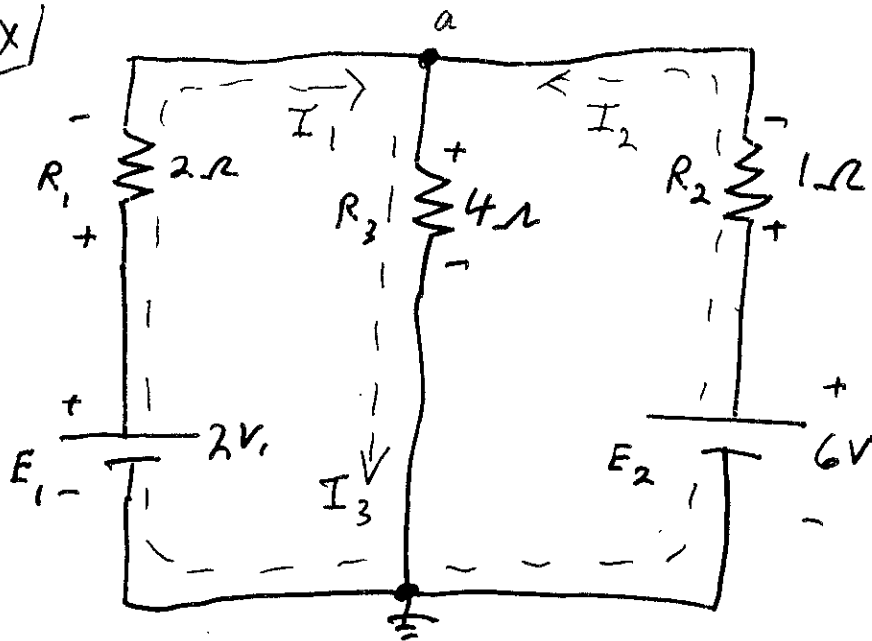


2 nodes
 $2 - 1 = 1 \text{ eqn.}$



4 nodes
 $4 - 1 = 3 \text{ eqns.}$

ex/



Solve by
branch-current
method

Solution:

- 1.) Assign currents I_1, I_2, I_3
- 2.) Label Voltage polarities across resistors
- 3.) Apply KVL to 2 closed loops.

$$\text{Loop 1: } +E_1 - V_{R_3} - V_{R_1} = 0$$

$$2 - V_{R_3} - V_{R_1} = 0$$

$$\text{Apply } \Omega \text{ Law: } V_{R_3} = (4\Omega)(I_3) \text{ and } V_{R_1} = (2\Omega)(I_1)$$

$$\text{substitute into KVL: } 2 - 4I_3 - 2I_1 = 0 \leftarrow \text{eqn. (1)}$$

$$\text{Loop 2: } +E_2 - V_{R_3} - V_{R_2} = 0$$

$$6 - V_{R_3} - V_{R_2} = 0$$

$$\text{Apply } \Omega \text{ Law: } V_{R_3} = (4\Omega)(I_3) \text{ and } V_{R_2} = (1\Omega)(I_2)$$

$$\text{substitute into KVL: } 6 - 4I_3 - I_2 = 0 \leftarrow \text{eqn. (2)}$$

4.) Apply KCL at node a.

$$I_1 + I_2 = I_3 \quad \leftarrow \text{eqn. (3)}$$

5.) Solve equations (1), (2) and (3) simultaneously

$$2 - 4I_3 - 2I_1 = 0$$

$$6 - 4I_3 - I_2 = 0$$

$$I_1 + I_2 = I_3$$

Rewritten:

→

$$2I_1 + 0 + 4I_3 = 2$$

→

$$0 + I_2 + 4I_3 = 6$$

→

$$I_1 + I_2 - I_3 = 0$$

A system of 3 eqns. & 3 unknowns can be solved using Cramer's Rule.

$$I_1 = \frac{\begin{vmatrix} 2 & 0 & 4 \\ 6 & 1 & 4 \\ 0 & 1 & -1 \end{vmatrix}}{\begin{vmatrix} 2 & 0 & 4 \\ 0 & 1 & 4 \\ 1 & 1 & -1 \end{vmatrix}} = \frac{(2)(1)(-1) + (6)(1)(4) + (0)(4)(0) - [0 + 0 + 8]}{-2 + 0 + 0 - [4 + 8 + 0]} = \boxed{-1A}$$

$$I_2 = \frac{\begin{vmatrix} 2 & 2 & 4 \\ 0 & 6 & 4 \\ 1 & 0 & 1 \end{vmatrix}}{\begin{vmatrix} 2 & 0 & 4 \\ 0 & 1 & 4 \\ 1 & 1 & -1 \end{vmatrix}} = \boxed{2A}$$

$$I_3 = \frac{\begin{vmatrix} 2 & 0 & 2 \\ 0 & 1 & 6 \\ 1 & 1 & 0 \end{vmatrix}}{\begin{vmatrix} 2 & 0 & 4 \\ 0 & 1 & 4 \\ 1 & 1 & -1 \end{vmatrix}} = \boxed{1A}$$

a minus sign indicates the actual current flows in the opposite direction to the arrow on the schematic.

Cramer's Rule

Given a set of simultaneous, linear equations written in matrix form as $AX = B$, let $\Delta = \det A$.

Define Δ_i to be the determinant of the matrix that is obtained by replacing the i th column of A with the column comprising B .

Then

$$X_i = \frac{\Delta_i}{\Delta}$$

ex | Given equations: $X_1 - 2X_2 = 28$ Find X_1 and X_2
 $4X_1 + 6X_2 = 21$

This can be expressed as a matrix equation: $AX = B$

$$\begin{bmatrix} 1 & -2 \\ 4 & 6 \end{bmatrix} \begin{bmatrix} X_1 \\ X_2 \end{bmatrix} = \begin{bmatrix} 28 \\ 21 \end{bmatrix}$$

First find $\Delta = \det A = \begin{vmatrix} 1 & -2 \\ 4 & 6 \end{vmatrix} = 6 - (-8) = 14$

Replacing the first column of A by the column comprising B , we get:

$$\Delta_1 = \begin{vmatrix} 28 & -2 \\ 21 & 6 \end{vmatrix} = 168 - (-42) = 210$$

Thus $X_1 = \frac{\Delta_1}{\Delta} = \frac{210}{14} = \boxed{15}$

Similarly: $\Delta_2 = \begin{vmatrix} 1 & 28 \\ 4 & 21 \end{vmatrix} = 21 - 112 = -91$

Then $X_2 = \frac{\Delta_2}{\Delta} = \frac{-91}{14} = \boxed{-\frac{13}{2}}$

EXPANDING DETERMINANTS

For 2×2 matrix

$$A = \begin{bmatrix} a & c \\ b & d \end{bmatrix} \quad |A| = \begin{vmatrix} a & c \\ b & d \end{vmatrix} = ad - bc$$

EX.

$$A = \begin{bmatrix} 1 & 2 \\ 3 & 4 \end{bmatrix} \quad |A| = (1)(4) - (3)(2) = 4 - 6 = -2$$

$$B = \begin{bmatrix} -1 & 2 \\ 0 & 1 \end{bmatrix} \quad |B| = -1(1) - 2(0) = -1$$

FOR 3×3 matrix

EXPAND ALONG TOP ROW
3 2×2 det.

$$A = \begin{bmatrix} a & b & c \\ d & e & f \\ g & h & i \end{bmatrix}$$

1st. strike 1st row & Column mult. by a

$$\begin{vmatrix} \cancel{a} & \cancel{b} & \cancel{c} \\ d & e & f \\ g & h & i \end{vmatrix} = a \begin{vmatrix} e & f \\ h & i \end{vmatrix}$$

2nd strike 1st row & 2nd Column... mult. by $-b$

$$\begin{vmatrix} \cancel{a} & \cancel{b} & c \\ d & e & f \\ g & h & i \end{vmatrix} = a \begin{vmatrix} e & f \\ h & i \end{vmatrix} - b \begin{vmatrix} d & f \\ g & i \end{vmatrix}$$

EXPANDING DETERMINANTS

3rd step 3x3 matrix

strike 1st row & 3rd column mult by c

$$\begin{vmatrix} \cancel{a} & \cancel{b} & \cancel{c} \\ d & e & f \\ g & h & i \end{vmatrix} = a \begin{vmatrix} e & f \\ h & i \end{vmatrix} - b \begin{vmatrix} d & f \\ g & i \end{vmatrix} + c \begin{vmatrix} d & e \\ g & h \end{vmatrix}$$

expand 2x2 det. and simplify

Ex.

$$\begin{vmatrix} 3 & 0 & -1 \\ 2 & 4 & 3 \\ -1 & 2 & 2 \end{vmatrix} = 3 \begin{vmatrix} 4 & 3 \\ 2 & 2 \end{vmatrix} - 0 \begin{vmatrix} 2 & 3 \\ -1 & 2 \end{vmatrix} - 1 \begin{vmatrix} 2 & 4 \\ -1 & 2 \end{vmatrix}$$

$$= 3(4(2) - 3(2)) - 0(2(2) - (-1)(3)) - 1(2(2) - (4)(-1))$$

$$= 3(8 - 6) - 0 - 1(4 + 4)$$

$$= 3(2) - 8$$

$$= \underline{\underline{-2}}$$

Ex

$$\begin{vmatrix} 3 & -2 & 1 \\ 0 & 2 & 1 \\ -1 & 0 & 1 \end{vmatrix} = 3 \begin{vmatrix} 2 & 1 \\ 0 & 1 \end{vmatrix} - (-2) \begin{vmatrix} 0 & 1 \\ -1 & 1 \end{vmatrix} + 1 \begin{vmatrix} 0 & 2 \\ -1 & 0 \end{vmatrix}$$

$$= 3[2(1) - (0)(1)] + 2[0(1) - (-1)(1)] + 1[0(0) - (2)(-1)]$$

$$= 3[2] + 2[1] + [2](1)$$

$$= 6 + 2 + 2 = \underline{\underline{10}}$$

ex | Given equations: $2x_1 - 3x_2 - 7x_3 = 5$

Find x_1, x_2, x_3

by Cramer's Rule.

$$5x_1 + x_2 = -2$$

$$-8x_1 + 2x_2 + 7x_3 = 1$$

matrix form:

$$AX = B$$

First find $\Delta = \det A$

$$\begin{bmatrix} 2 & -3 & -7 \\ 5 & 1 & 0 \\ -8 & 2 & 7 \end{bmatrix} \begin{bmatrix} x_1 \\ x_2 \\ x_3 \end{bmatrix} = \begin{bmatrix} 5 \\ -2 \\ 1 \end{bmatrix}$$

$$\begin{aligned} \Delta &= \begin{vmatrix} 2 & -3 & -7 \\ 5 & 1 & 0 \\ -8 & 2 & 7 \end{vmatrix} = (2)(1)(7) + (-3)(-8)(0) + (-7)(5)(2) \\ &\quad - [(2)(0)(2) + (7)(-3)(5) + (-7)(1)(-8)] \\ &= 14 + 0 - 70 - [0 - 105 + 56] \\ &= -56 + 49 = -7 \end{aligned}$$

$$\text{Then } \Delta_1 = \begin{vmatrix} 5 & -3 & -7 \\ -2 & 1 & 0 \\ 1 & 2 & 7 \end{vmatrix} = 35 + 0 + 28 - [-7 + 0 + 42] = 28$$

$$\text{Thus } x_1 = \frac{\Delta_1}{\Delta} = \frac{28}{-7} = \boxed{-4}$$

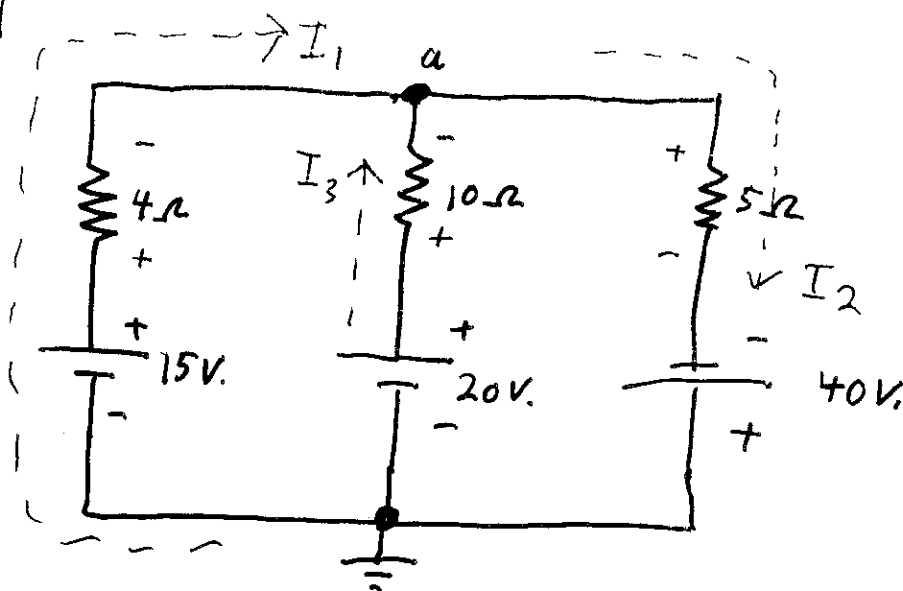
$$\text{Then } \Delta_2 = \begin{vmatrix} 2 & 5 & -7 \\ 5 & -2 & 0 \\ -8 & 1 & 7 \end{vmatrix} = -28 + 0 - 35 - [-112 + 0 + 175] = -126$$

$$\text{Thus } x_2 = \frac{\Delta_2}{\Delta} = \frac{-126}{-7} = \boxed{18}$$

$$\text{Then } \Delta_3 = \begin{vmatrix} 2 & -3 & 5 \\ 5 & 1 & -2 \\ -8 & 2 & 1 \end{vmatrix} = 2 - 48 + 50 - (-40 - 8 - 15) = 67$$

$$\text{Finally } x_3 = \frac{\Delta_3}{\Delta} = \frac{67}{-7} = \boxed{-\frac{67}{7}}$$

ex/



Solve by
Branch-current
Method

Solution: 1.) Assign currents I_1, I_2, I_3 (arbitrary $\rightarrow$)
2.) Label voltage polarities across resistors
(+ on side I enters)

3.) Apply KVL to 2 closed loops.

$$\text{Loop 1: } -10 I_3 + 20 - 15 + 4 I_1 = 0$$

$$4 I_1 + 0 - 10 I_3 = -5 \quad \text{eqn. (1)}$$

$$\text{Loop 2: } 5 I_2 - 40 - 20 + 10 I_3 = 0$$

$$0 + 5 I_2 + 10 I_3 = 60 \quad \text{eqn. (2)}$$

4.) Apply KCL at node a

$$I_1 + I_3 = I_2 \quad \text{eqn. (3)}$$

5.) Solve equations (1), (2) and (3) simultaneously

Cramer's rule could be used or we can first solve eqn (3) for I_2 and then substitute I_2 into eqn. (2) to get 2 eqns. and 2 unknowns.

$$I_2 = I_1 + I_3$$

substituting:

$$5(I_1 + I_3) + 10I_3 = 60 \quad \text{eqn. (2)}$$

$$5I_1 + 15I_3 = 60$$

Solve these 2 eqns. simultaneously

$$\begin{cases} I_1 + 3I_3 = 12 \\ 4I_1 - 10I_3 = -5 \end{cases} \leftarrow \text{eqn (1)}$$

$$I_1 = \frac{\begin{vmatrix} 12 & 3 \\ -5 & -10 \end{vmatrix}}{\begin{vmatrix} 1 & 3 \\ 4 & -10 \end{vmatrix}} = \frac{-120 - [-15]}{-10 - 12} = \frac{-105}{-22} = \boxed{4.773 \text{ A.}}$$

$$I_3 = \frac{\begin{vmatrix} 1 & 12 \\ 4 & -5 \end{vmatrix}}{\begin{vmatrix} 1 & 3 \\ 4 & -10 \end{vmatrix}} = \frac{-5 - 48}{-22} = \frac{-53}{-22} = \boxed{2.409 \text{ A.}}$$

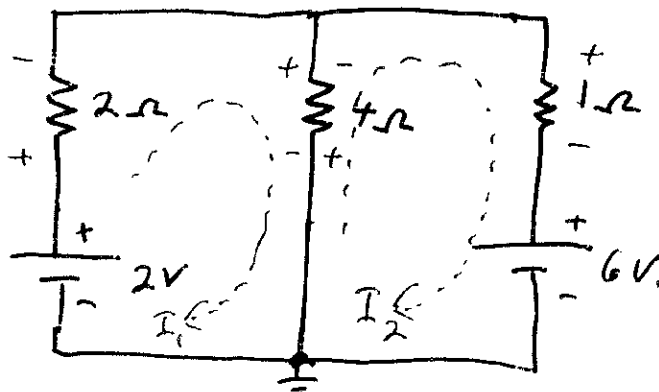
Then from eqn. (3)

$$I_2 = I_1 + I_3 = 4.773 + 2.409 = \boxed{7.182 \text{ A.}}$$

Mesh Analysis (General Approach)

1. Assign a clockwise current to each mesh. (closed loop)
2. Label voltage polarities across each resistor due to each mesh current.
(+ on side I enters R)
3. Apply KVL in clockwise direction around each mesh.
 - a.) For resistors shared by 2 meshes, the Total of both mesh currents must be used in ohms law calculation.
 - b.) Polarity of voltage sources is unaffected by mesh current directions
4. Solve the resulting set of equations for the assumed mesh currents.

ex)



Solve:

For mesh 1:
 $-2 + 2I_1 + 4(I_1 - I_2) = 0$
eqn. (1) $\Rightarrow 6I_1 - 4I_2 = 2$

For mesh 2:
 $6 + 4(I_2 - I_1) + I_2 = 0$
eqn. (2) $\Rightarrow -4I_1 + 5I_2 = -6$

(note sum of I thru 4Ω R)

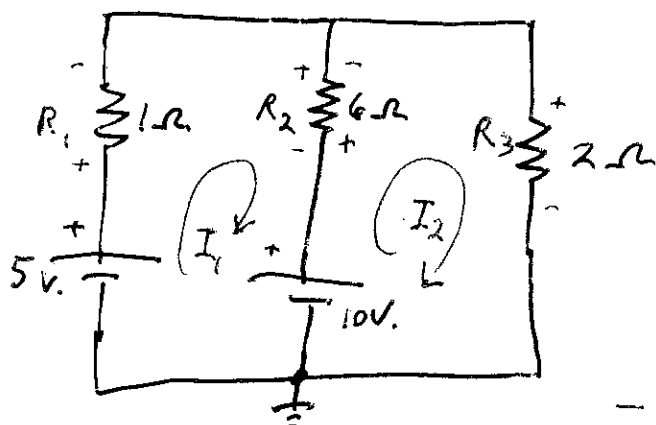
Solving with Cramer's Rule:

$$I_1 = \frac{\begin{vmatrix} 2 & -4 \\ -6 & 5 \end{vmatrix}}{\begin{vmatrix} 6 & -4 \\ -4 & 5 \end{vmatrix}} = \frac{10 - 24}{30 - 16} = \frac{-14}{14} = \boxed{-1A}$$

$$I_2 = \frac{\begin{vmatrix} 6 & 2 \\ -4 & -6 \end{vmatrix}}{\begin{vmatrix} 6 & -4 \\ -4 & 5 \end{vmatrix}} = \frac{-36 + 8}{14} = \frac{-28}{14} = \boxed{-2A}$$

$$I_{4\Omega R} = I_1 - I_2 = -1 - (-2) = 1A$$

ex



Solve for branch currents:

Solution:

For mesh 1:

$$-5 + I_1 + 6(I_1 - I_2) + 10 = 0$$

$$7I_1 - 6I_2 = -5 \leftarrow \text{eqn. (1)}$$

For mesh 2:

$$2I_2 - 10 + 6(I_2 - I_1) = 0$$

$$-6I_1 + 8I_2 = 10$$

$$-3I_1 + 4I_2 = 5 \leftarrow \text{eqn. (2)}$$

$$I_1 = \frac{\begin{vmatrix} -5 & -6 \\ 5 & 4 \end{vmatrix}}{\begin{vmatrix} 7 & -6 \\ -3 & 4 \end{vmatrix}} = \frac{-20 + 30}{28 - 18} = \frac{10}{10} = \boxed{1A} = I_{R_1}$$

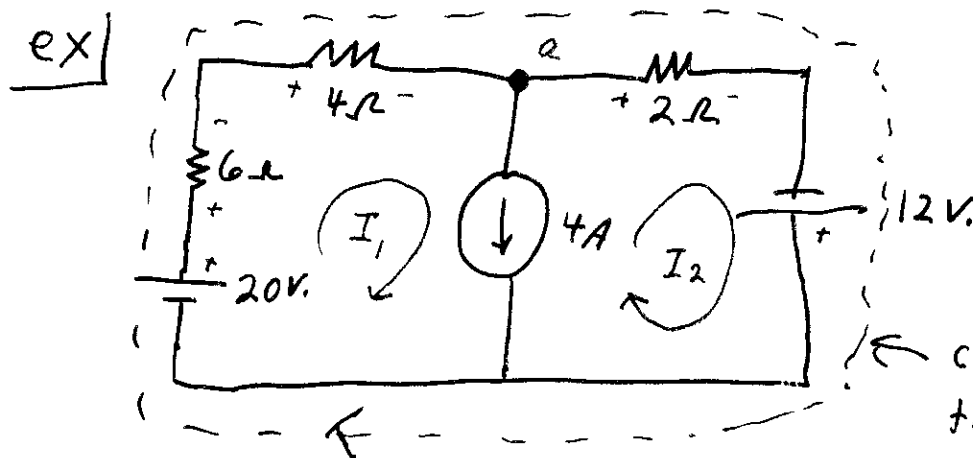
$$I_2 = \frac{\begin{vmatrix} 7 & -5 \\ -3 & 5 \end{vmatrix}}{10} = \frac{35 - 15}{10} = \boxed{2A} = I_{R_3}$$

$$I_{R_2} = I_2 - I_1 = 2 - 1 = \boxed{1A}$$

(in the direction of I_2)

Supermesh Currents

If there are current sources in the network, do not construct any KVL loops which include a current source. If necessary combine more than one mesh together to form a supermesh which avoids the current source in its path.



← consider supermesh to avoid current source

solution: 1.) create supermesh

2.) draw mesh currents I_1 & I_2

3.) write KVL around supermesh path:

$$-20 + 6I_1 + 4I_1 + 2I_2 - 12 = 0$$

$$10I_1 + 2I_2 = 32 \quad \leftarrow \text{eqn. (1)}$$

4.) Get needed 2nd equation by writing KCL at current source's node a.

$$I_1 = I_2 + 4$$

$$I_1 - I_2 = 4 \quad \leftarrow \text{eqn. (2)}$$

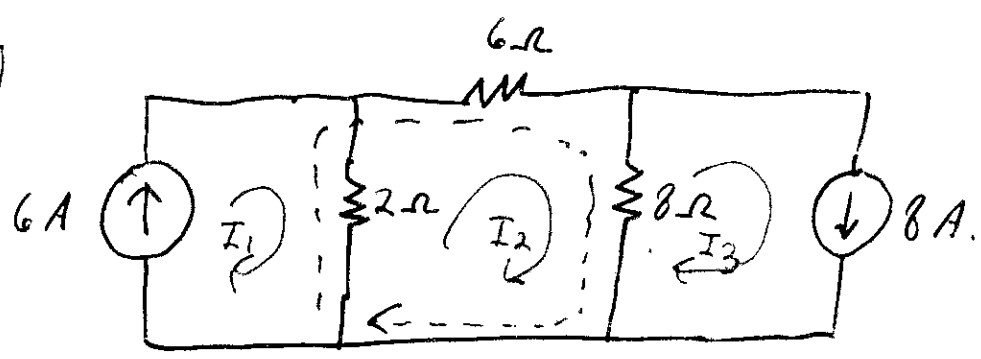
can have solved by using nodal analysis.

$$\left. \begin{aligned} 10 I_1 + 2 I_2 &= 32 \\ I_1 - I_2 &= 4 \end{aligned} \right\}$$

$$I_1 = \frac{\begin{vmatrix} 32 & 2 \\ 4 & -1 \end{vmatrix}}{\begin{vmatrix} 10 & 2 \\ 1 & -1 \end{vmatrix}} = \frac{-32 - 8}{-10 - 2} = \frac{-40}{-12} = \boxed{3.33 A}$$

$$I_2 = \frac{\begin{vmatrix} 10 & 32 \\ 1 & 4 \end{vmatrix}}{-12} = \frac{40 - 32}{-12} = \frac{8}{-12} = \boxed{-0.67 A}$$

ex)



Find network currents:

- 1.) Draw mesh currents
- 2.) Construct supermesh to avoid current sources.
- 3.) Write KVL around supermesh path

$$6 I_2 + 8 (I_2 - I_3) + 2 (I_2 - I_1) = 0$$

$$-2 I_1 + 16 I_2 - 8 I_3 = 0 \leftarrow \text{eqn ①}$$

- 4.) Since each current source only has one mesh current passing through it:

$$\boxed{I_1 = 6 A} \quad \boxed{I_3 = 8 A}$$

Solving eqn ① for I_2 :

$$16 I_2 = 2 I_1 + 8 I_3$$

$$I_2 = \frac{I_1}{8} + \frac{I_3}{2}$$

$$I_2 = \frac{6}{8} + \frac{8}{2} = \boxed{4.75 A}$$

Note: $I_{6\Omega} = I_2 = 4.75 A \rightarrow$

$I_{2\Omega} = I_1 - I_2 = 1.25 A \downarrow$

$I_{8\Omega} = I_3 - I_2 = 3.25 A \uparrow$